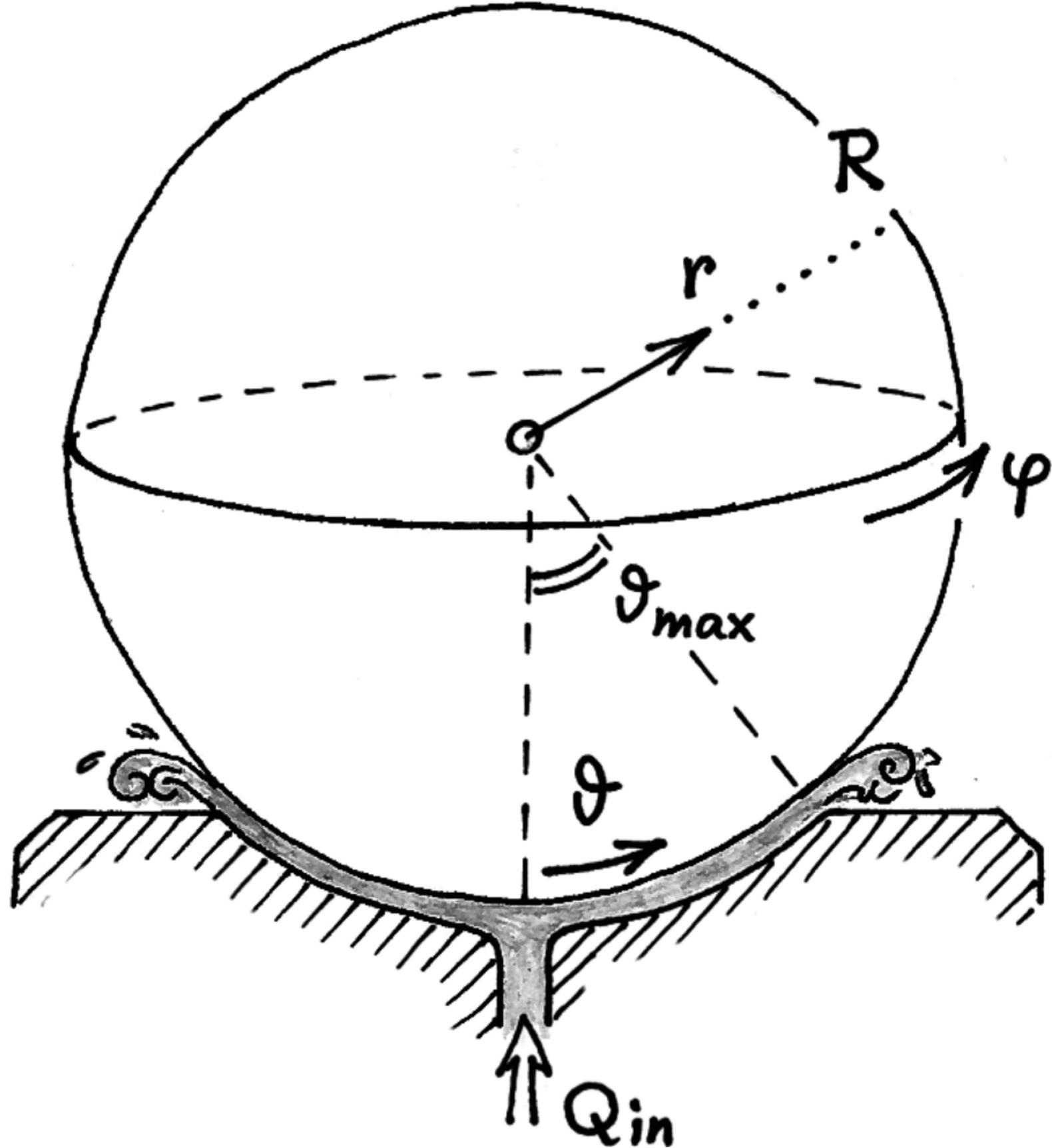


TRIBOLOGY OF WET SYSTEMS: FROM HYDRODYNAMIC TO BOUNDARY CONTACTS

- Introduction of lubricated contacts: hydrodynamic and boundary lubrication
- Connection between lubrication and rheology of concentrated suspensions (shear thickening)
- The impact of tribology beyond viscosity and flow curves
- Measuring single-particle friction
- Modifying boundary friction coefficients
- Open questions and interesting directions for future work

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$$F_g = F_{up} = \iint_{A_{sub}} [P(\theta) - P_{atm}] \cos \theta dA$$

$$m = (4/3)\pi R^3 \rho_{gr} = 1440 \text{ kg}$$

$$h_{sph} = \left[\frac{9}{2\pi} (1 - \cos \theta_{max}) \right]^{1/3} \left(\frac{\mu Q_{in}}{Rg\rho_{gr}} \right)^{1/3}$$

$$R = 0.5 \text{ m}$$

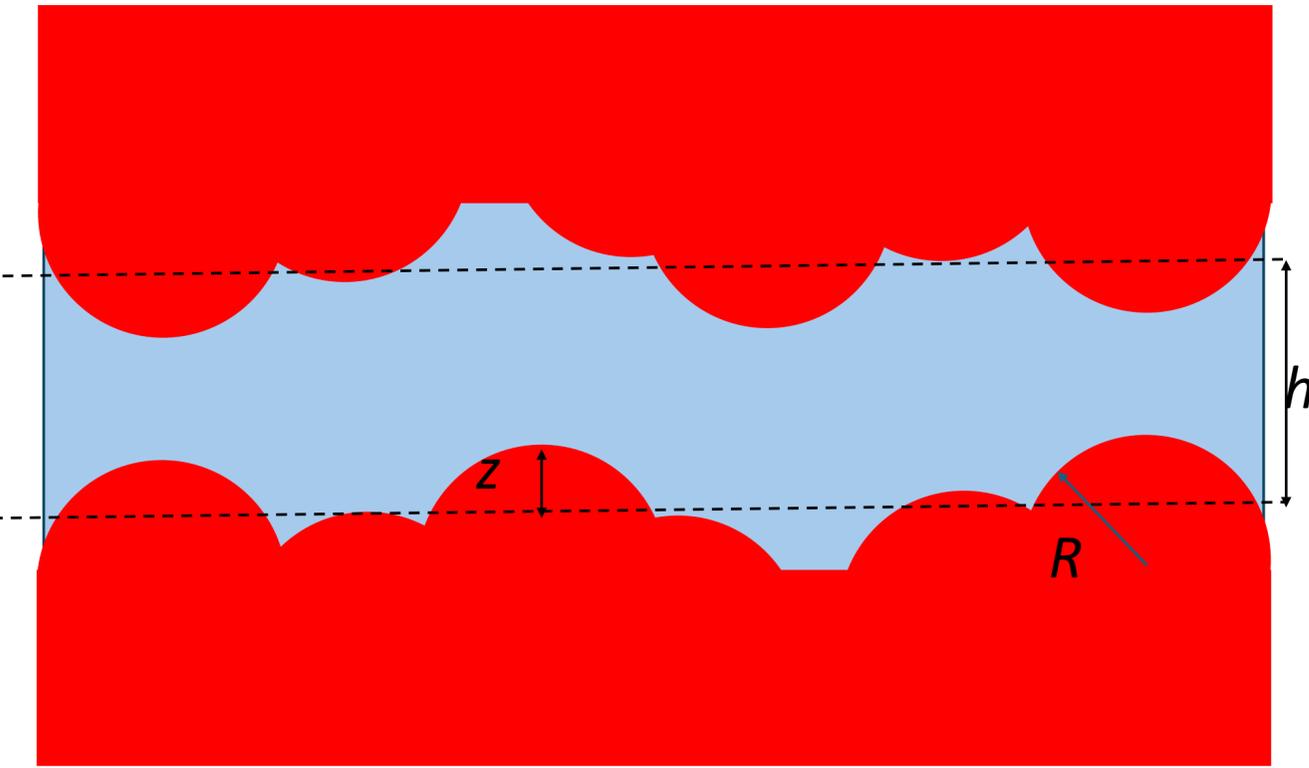
$$\theta_{max} = 0.6 \text{ rad}$$

$$\mu = 10^{-3} \text{ Pa s}$$

$$Q_{in} = 1.5 \text{ L/s}$$

$$\rho_{gr} = 2750 \text{ kg/m}^3$$

$$h_{sp} = 0.3 \text{ mm}$$

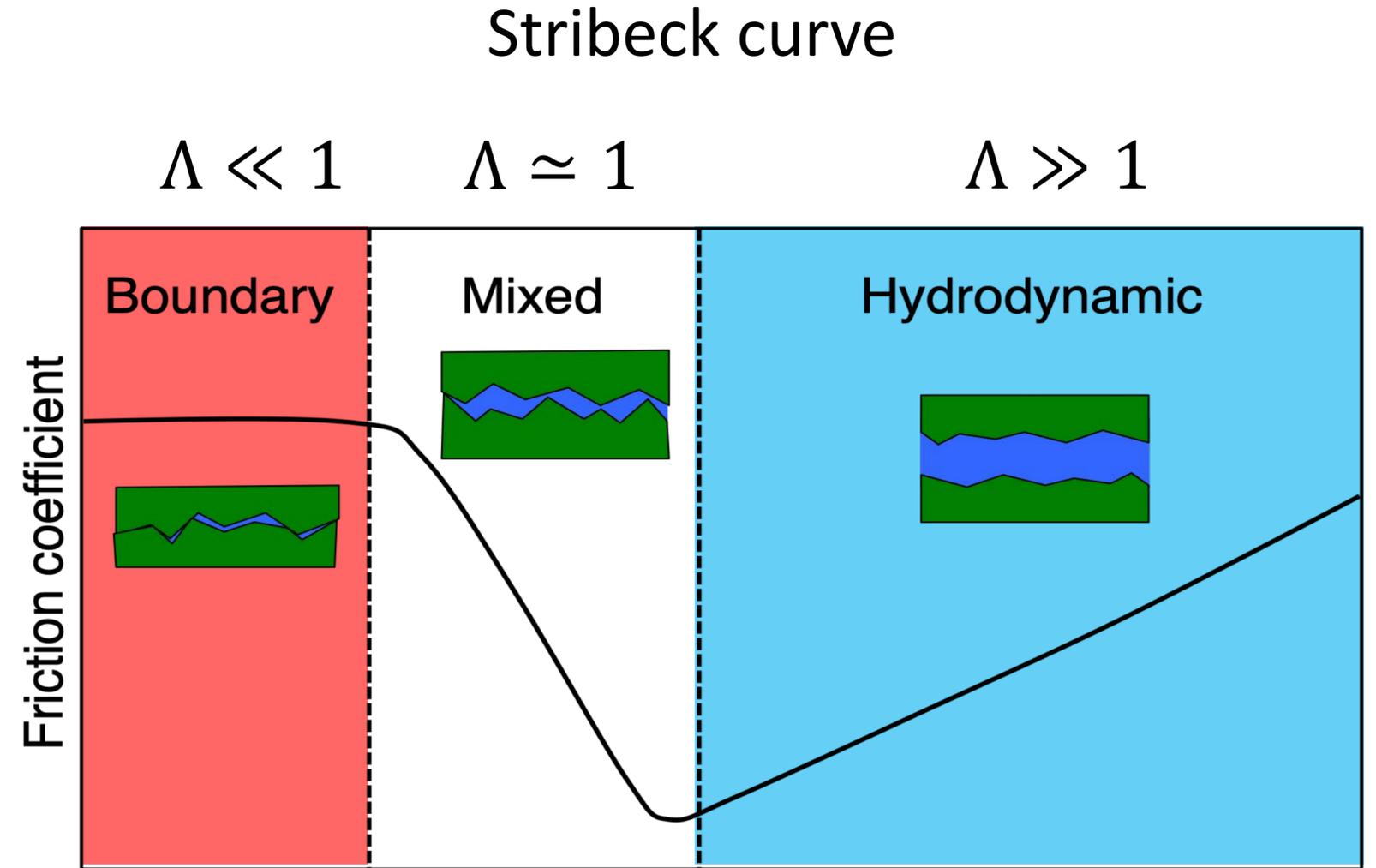


$$R_q = \sqrt{\frac{1}{L^2} \int_0^L \int_0^L (z(x, y) - z_0)^2 dx dy}$$

RMS roughness

$$\Lambda = \frac{h}{R_q}$$

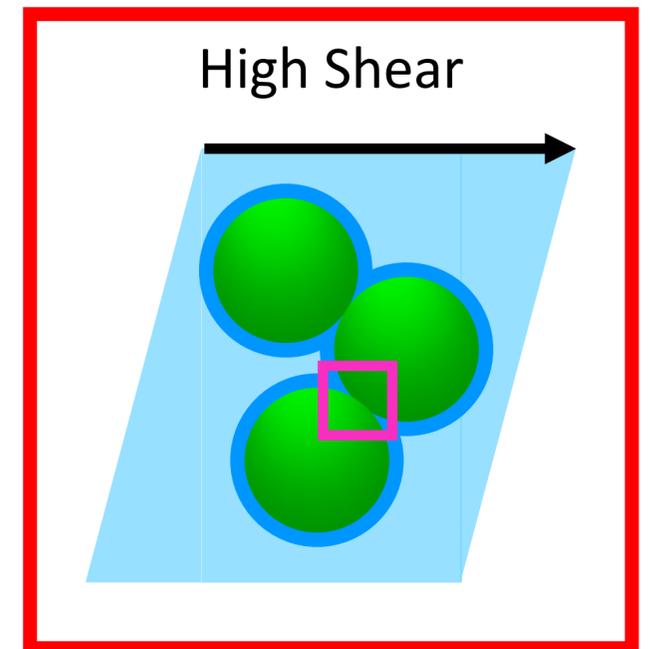
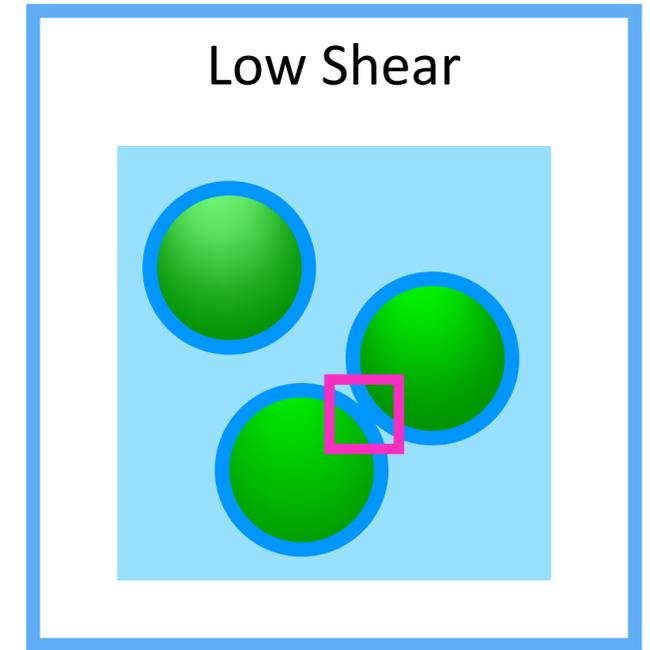
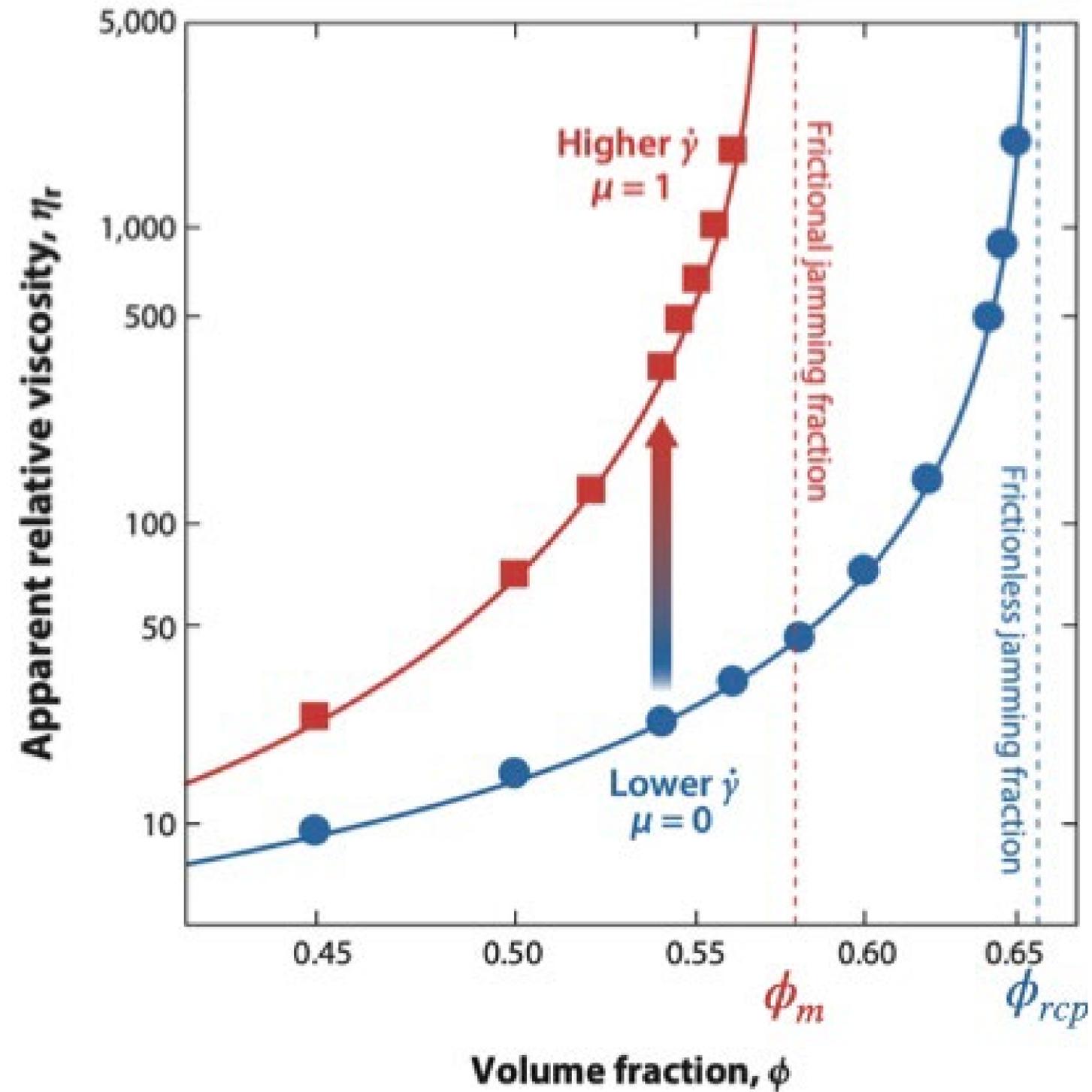
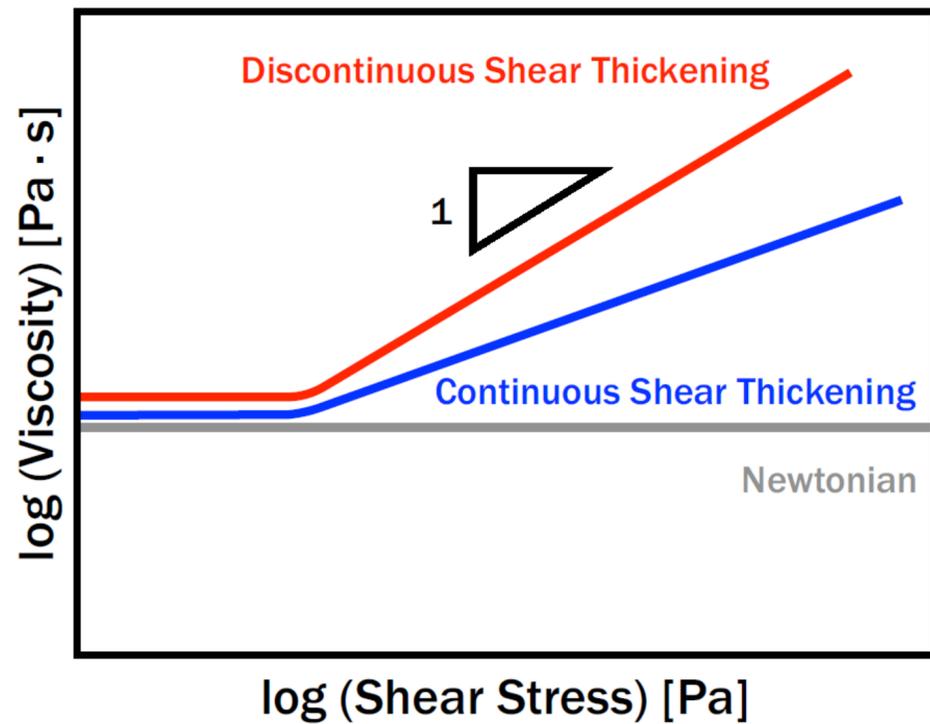
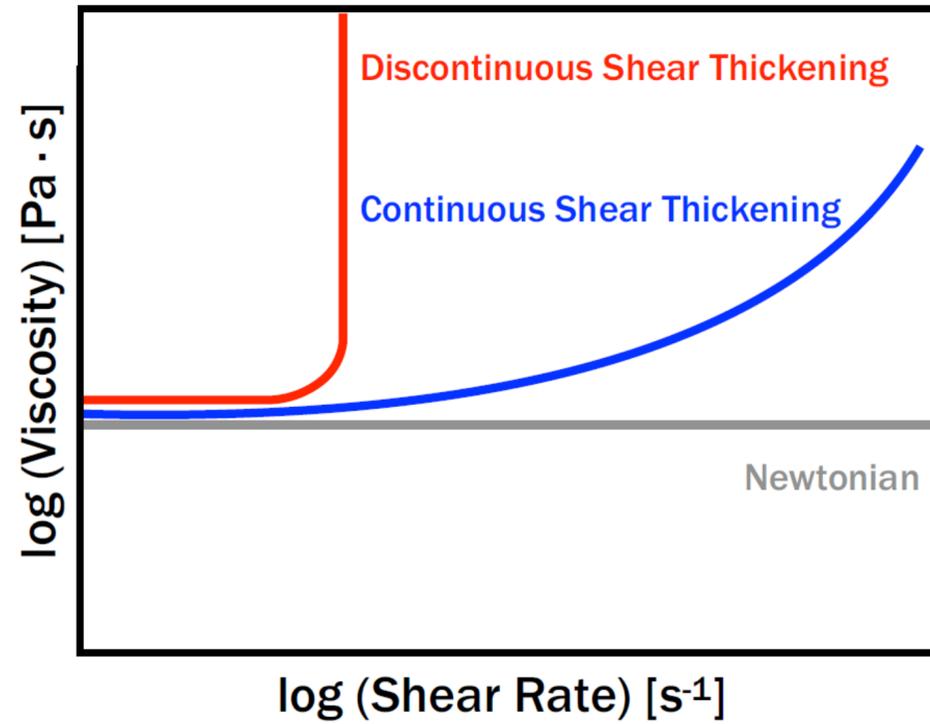
Lambda ratio



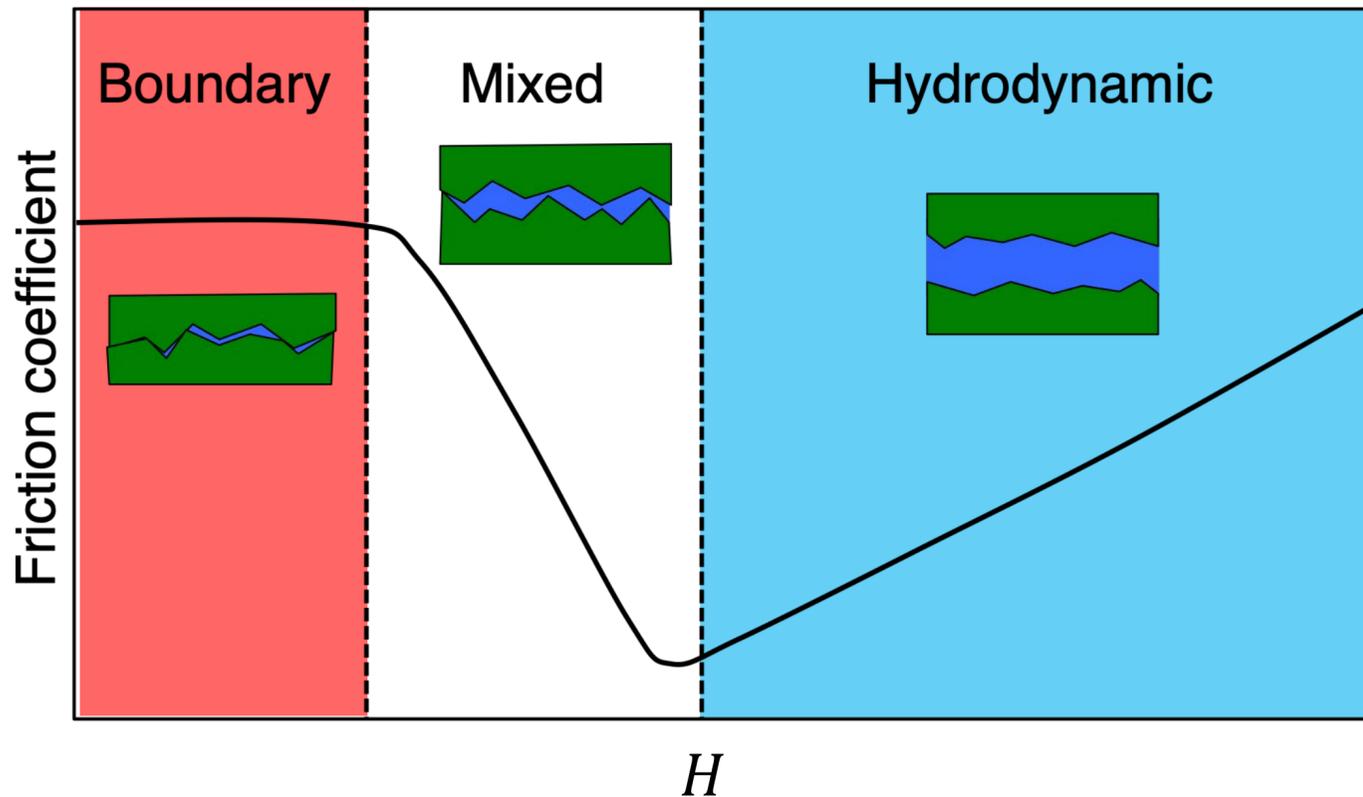
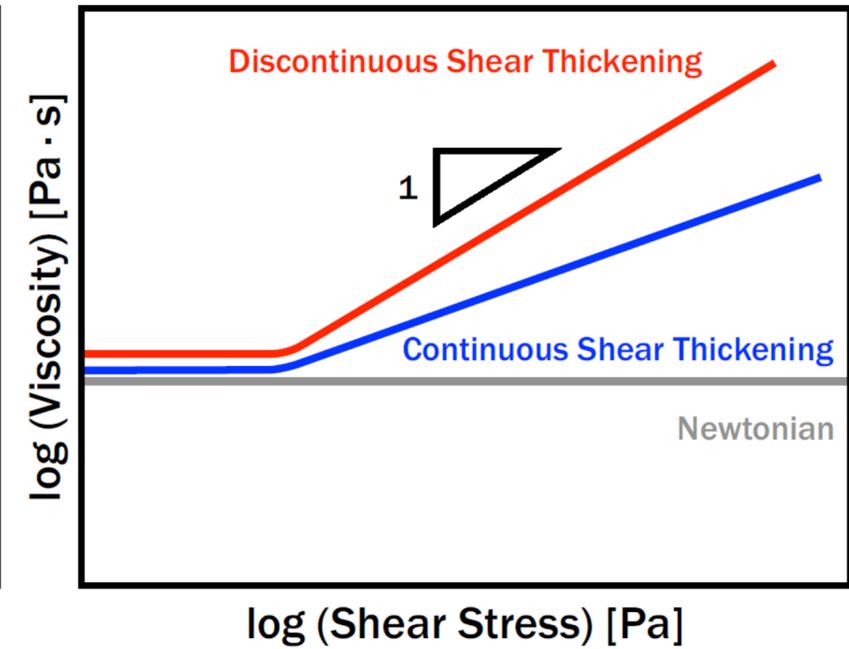
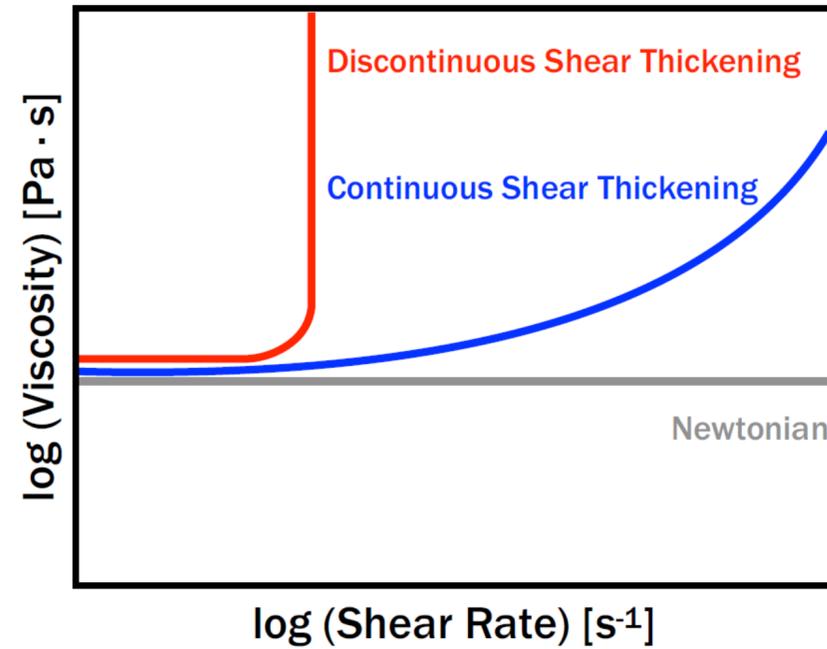
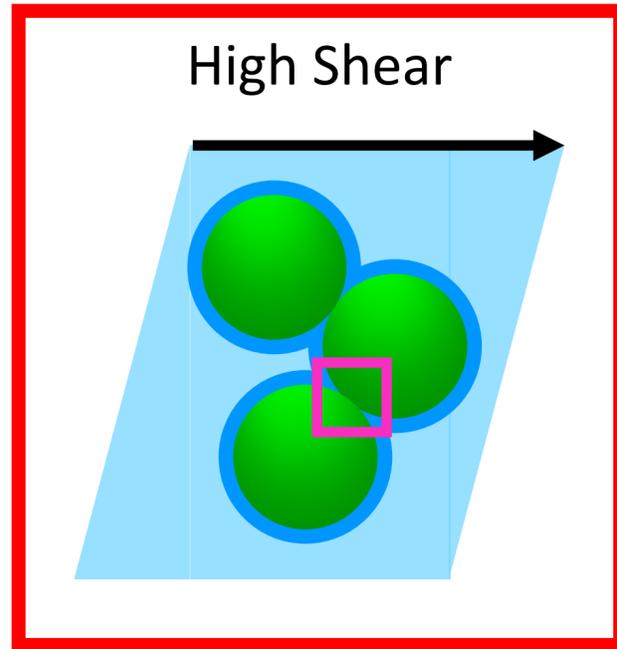
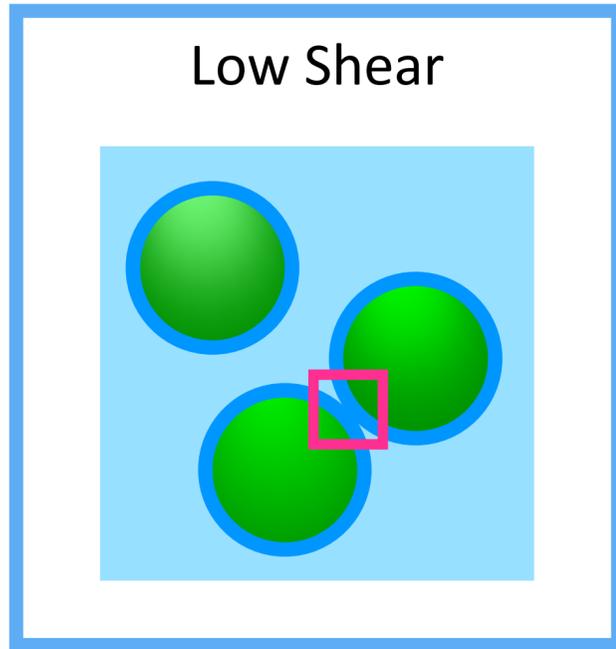
$$S \text{ or } H = \frac{\eta_f v a}{N}$$

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HYDRODYNAMIC-TO-BOUNDARY TRANSITION



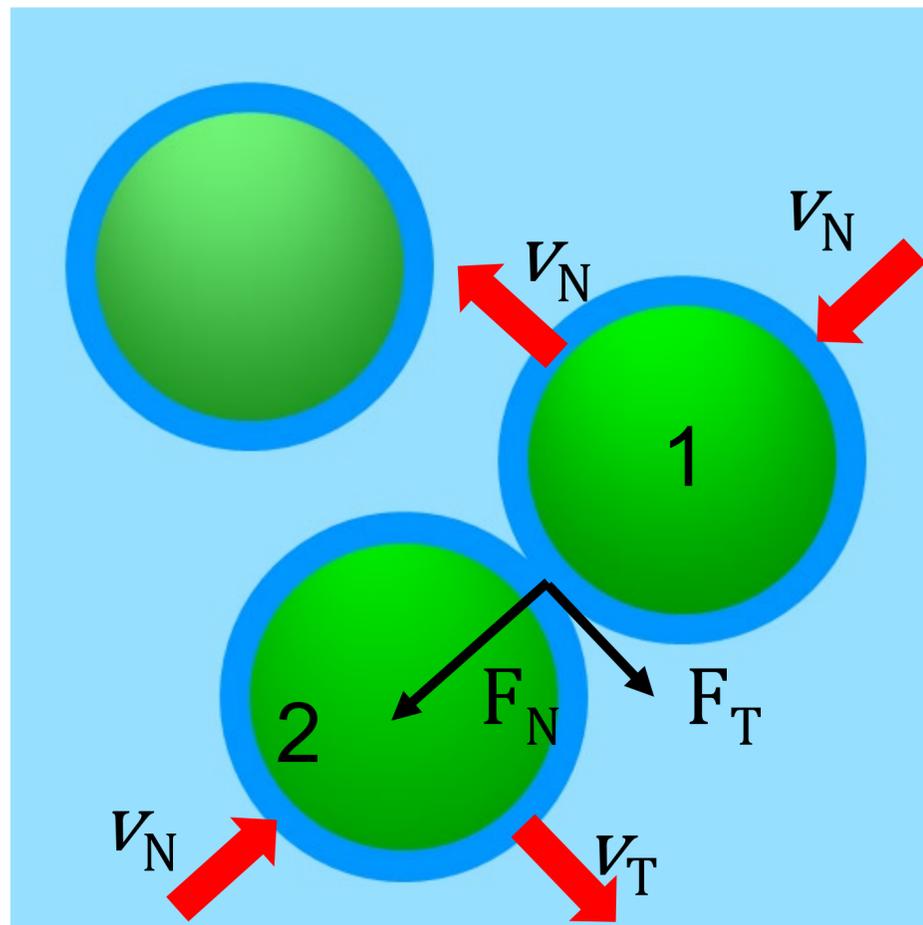
$$H = \frac{\eta_f v R_p}{N} = \frac{\eta_f \dot{\gamma}}{P_p}$$

$$P_p \propto \eta \dot{\gamma}$$

$$\eta = \eta_f \eta_0 \dot{\gamma}^{n-1}$$



$$H \propto \frac{1}{\eta_0 \dot{\gamma}^{n-1}}$$



$$\mathbf{F}_{1 \rightarrow 2}^{HD} = \frac{\pi}{10} \eta_f R_p \begin{bmatrix} -15h^{-1} & 12h^{-\frac{1}{2}} \\ 0 & -10 \ln(h^{-1}) \end{bmatrix} \begin{bmatrix} v_N \\ v_T \end{bmatrix}$$

Hydrodynamic forces diverge at contact



Cut-off distance for hydrodynamic to boundary transition



Inertia
(Large particles)
Fernandez et al PRL 2013

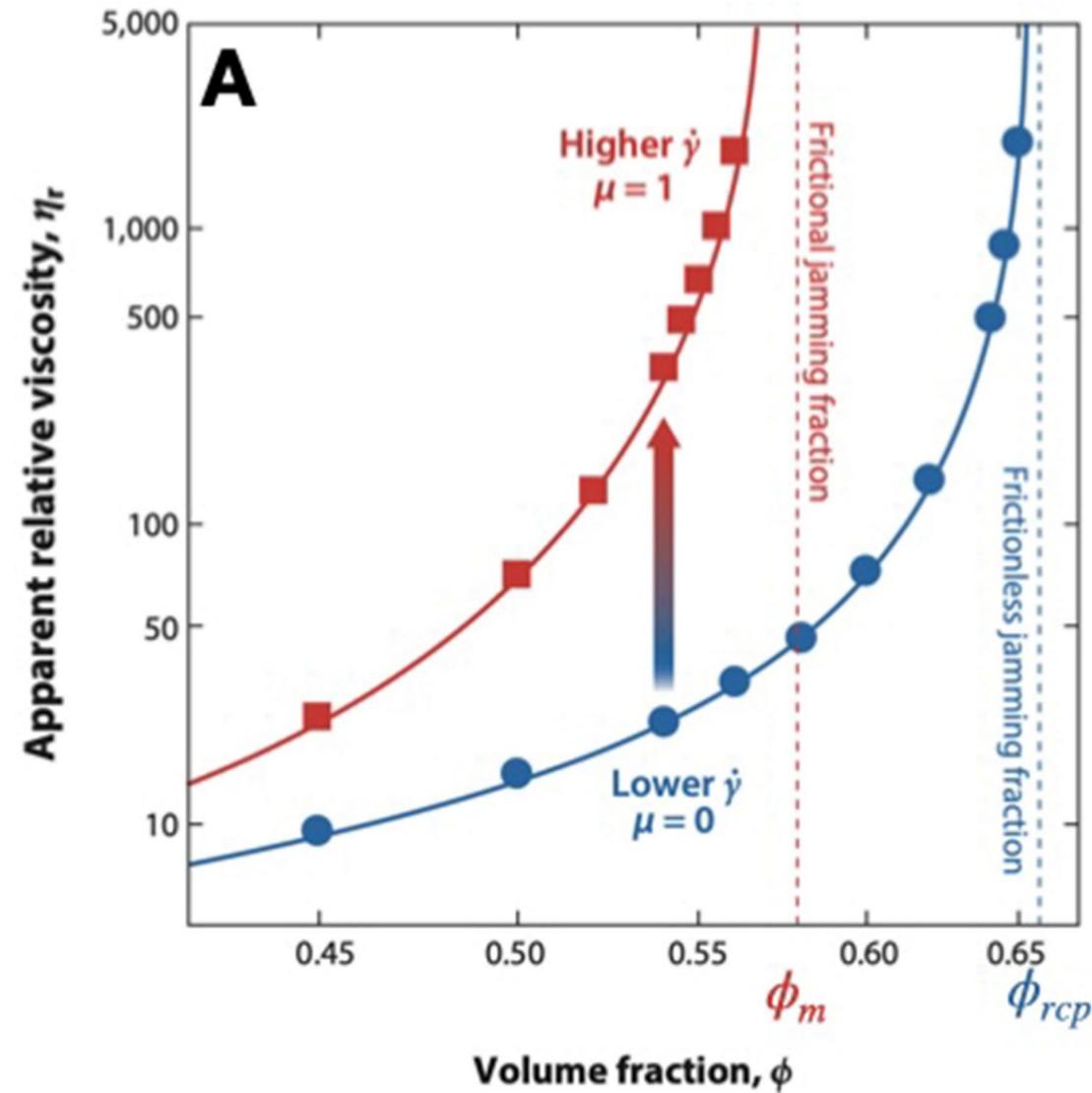


Overcoming a potential barrier
(e.g. charge-stabilized particles)
distance for which $P=P^*$
Wyart & Cates PRL 2014



Surface roughness

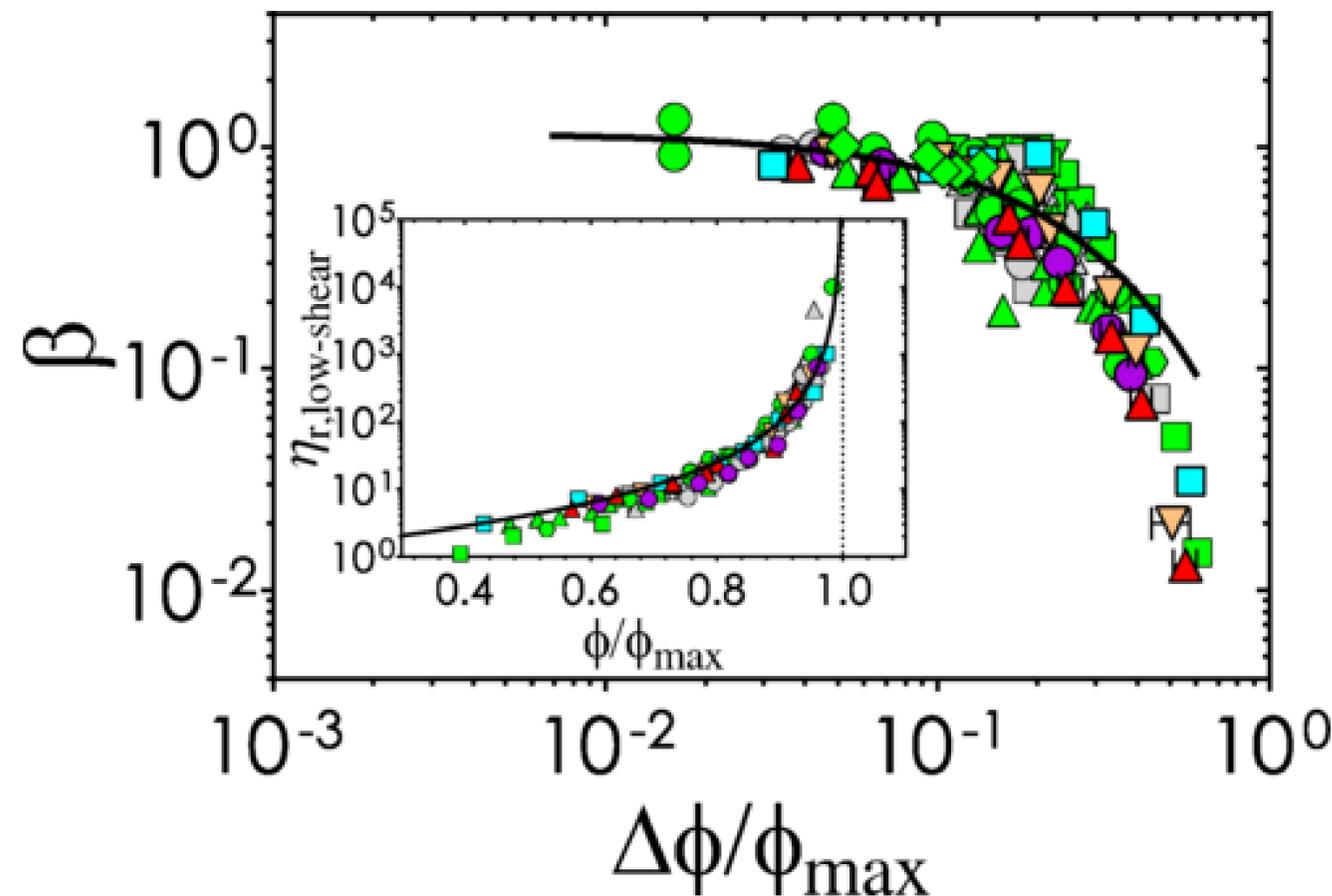
$$\Lambda = \frac{h}{R_q} \approx 1$$



PHYSICAL REVIEW LETTERS 127, 158002 (2021)

Jamming Distance Dictates Colloidal Shear Thickening

Shravan Pradeep¹, Mohammad Nabizadeh², Alan R. Jacob¹, Safa Jamali², and Lilian C. Hsiao^{1,*}



“...colloids with surface asperities interacting via lubrication (square) [11], spheres with sliding friction (upper triangle) [22], spheres with sliding and rolling friction (circle) [19]...”

$$\eta \propto (\phi_m - \phi)^{-2}$$

and

$$\phi_m = \phi_m(\mu)$$

Friction Coefficient

PHYSICAL REVIEW LETTERS 121, 128001 (2018)

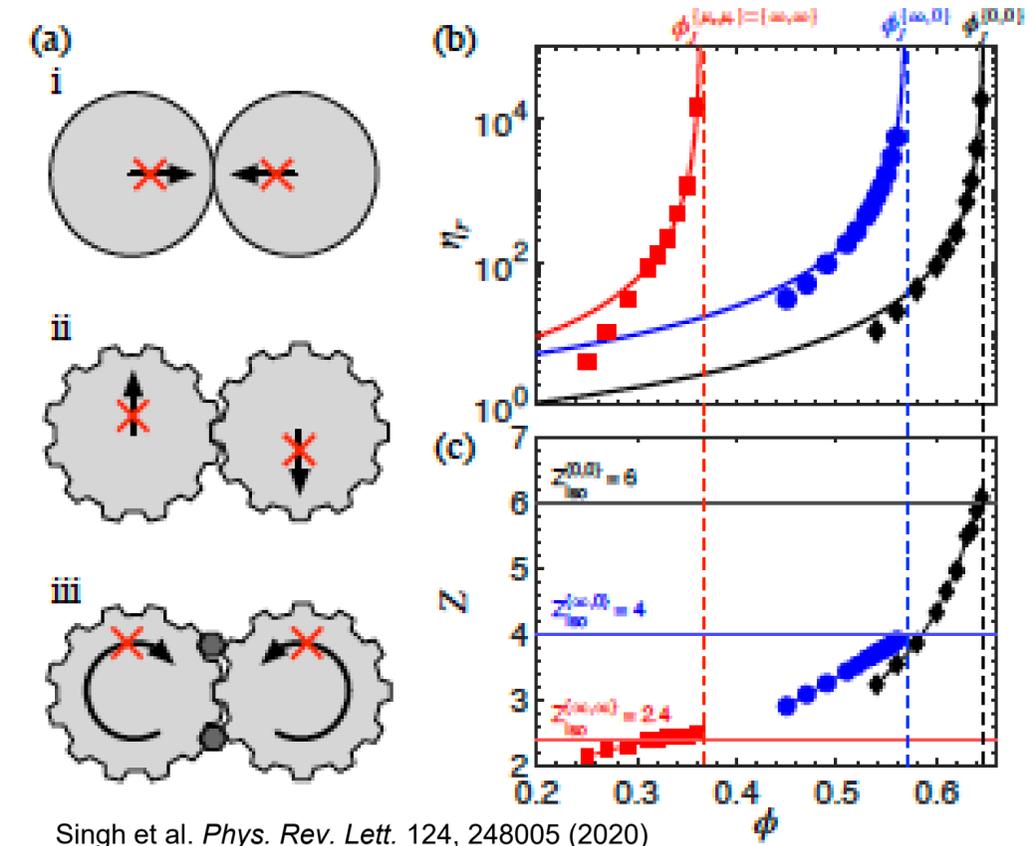
Constraint-Based Approach to Granular Dispersion Rheology

B. M. Guy,^{*} J. A. Richards,[†] D. J. M. Hodgson, E. Blanco, and W. C. K. Poon
 SUPA, School of Physics and Astronomy, The University of Edinburgh,
 King's Buildings, Peter Guthrie Tait Road, Edinburgh EH9 3FD, United Kingdom

(Received 10 May 2018; published 17 September 2018)

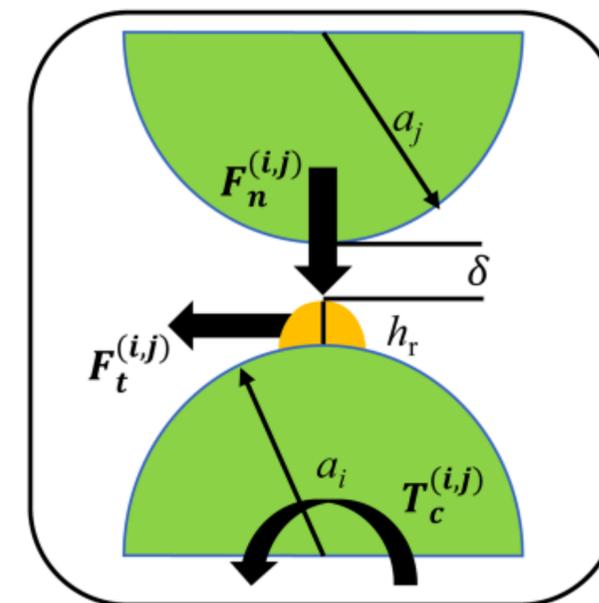
We present a phenomenological model for granular suspension rheology in which particle interactions enter as constraints to relative particle motion. By considering constraints that are *formed* and *released* by stress respectively, we derive a range of experimental flow curves in a single treatment and predict singularities in viscosity and yield stress consistent with literature data. Fundamentally, we offer a generic description of suspension flow that is independent of bespoke microphysics.

DOI: [10.1103/PhysRevLett.121.128001](https://doi.org/10.1103/PhysRevLett.121.128001)

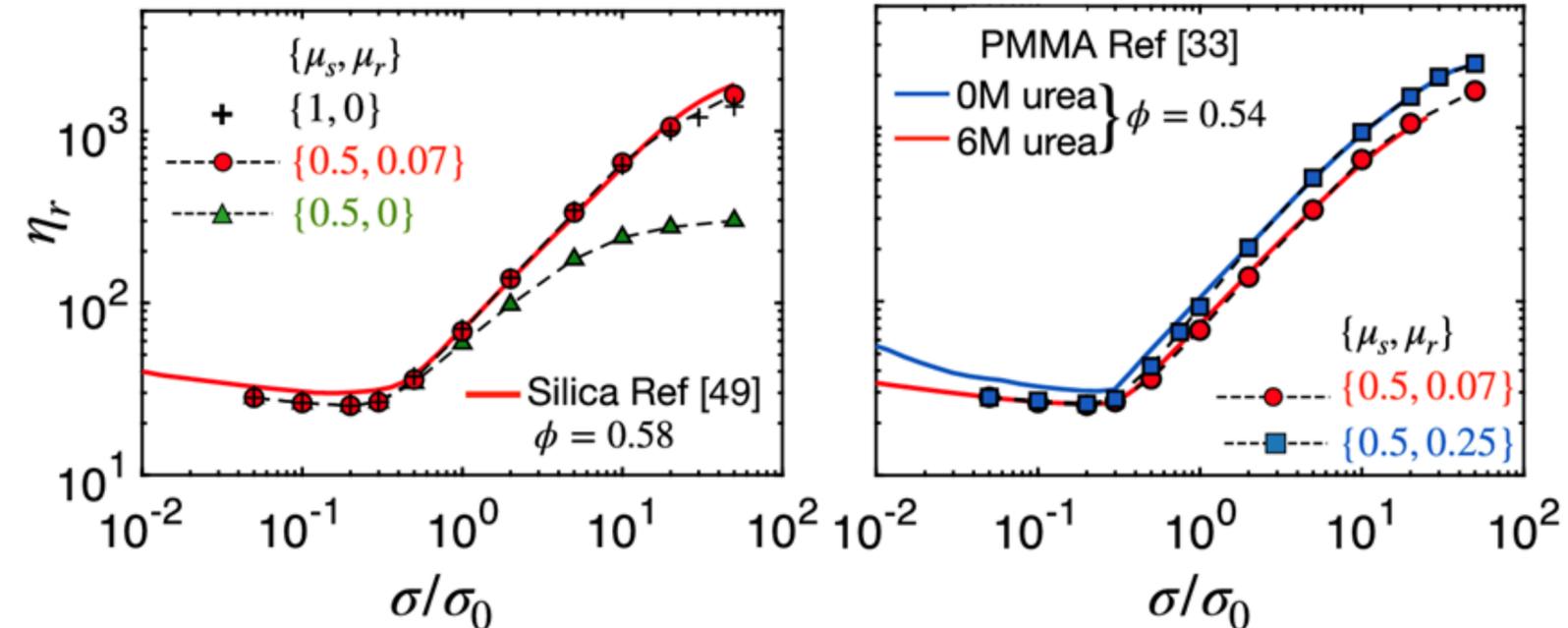
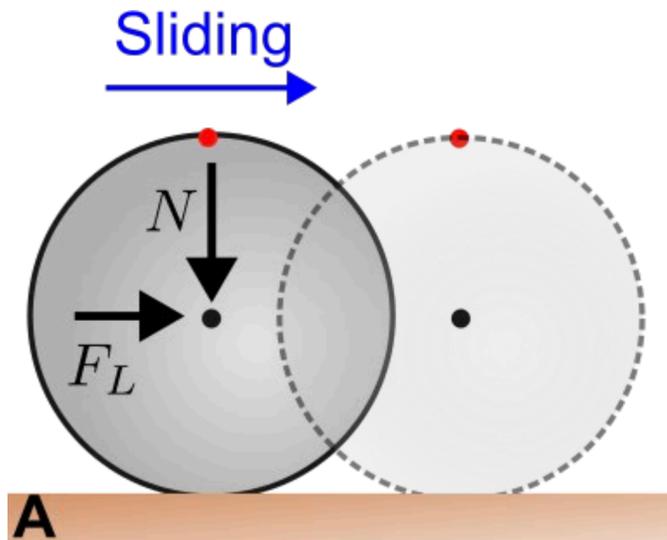


Singh et al. *Phys. Rev. Lett.* 124, 248005 (2020)

- There is a mapping between the friction coefficient and ϕ_m
- ϕ_m depends on the details of the frictional contact



Moore and Ardekani, *J. Rheol.* 64, 1107 (2020)



A. Singh *et al.*, PRL (2020)

$$F_L = \mu_s N + F_L^0$$

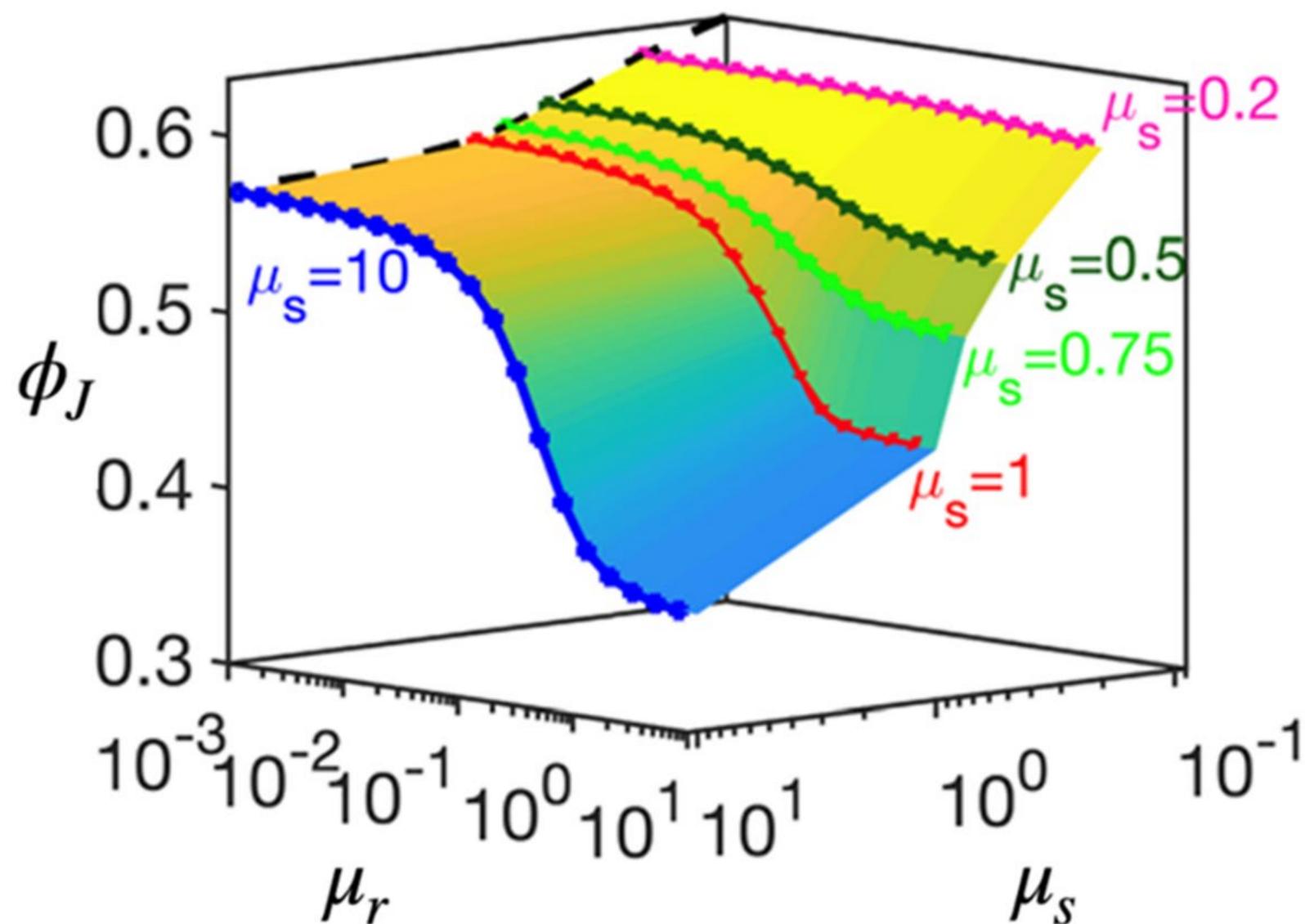
$$M = \lambda N + M^0$$

Friction force
 Sliding friction coefficient (dynamic)
 Normal load
 Friction force at zero load (adhesion)

$$\frac{M}{R_p} = \mu_R N + \frac{M^0}{R_p}$$

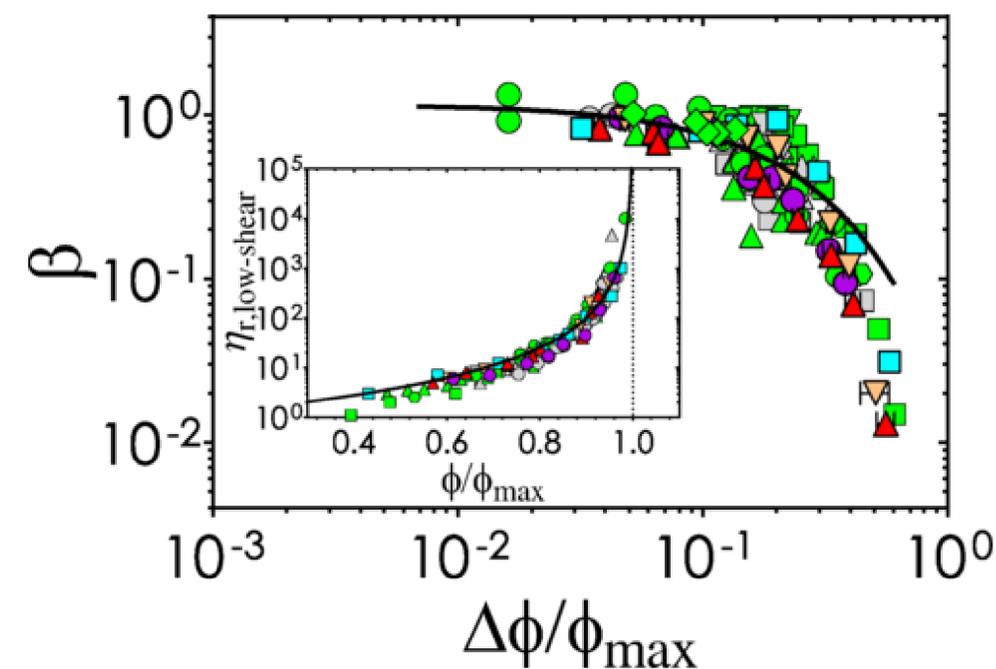
Particle radius
 Rolling friction coefficient (dynamic)

The rheology is defined by a combination of μ_s and μ_R



μ_s and μ_r determine ϕ_m

The distance from ϕ_m determines η



S. Pradeep *et al.*, **Phys. Rev. Lett.** (2021)

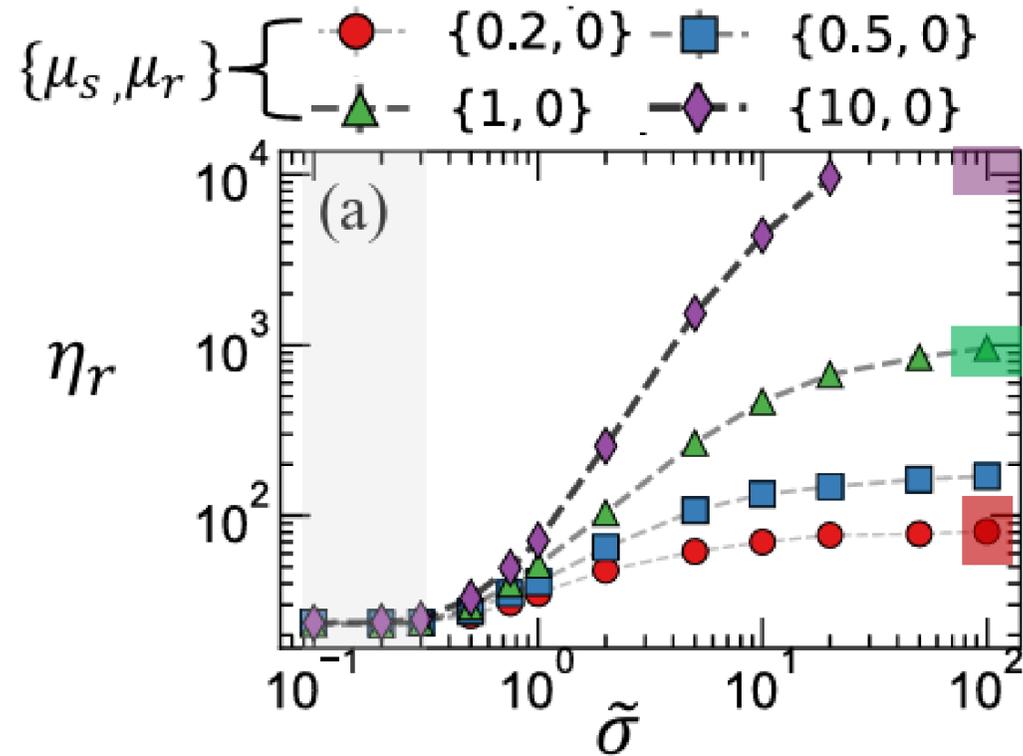
A. Singh *et al.*, **Phys. Rev. Fluids** (2022)

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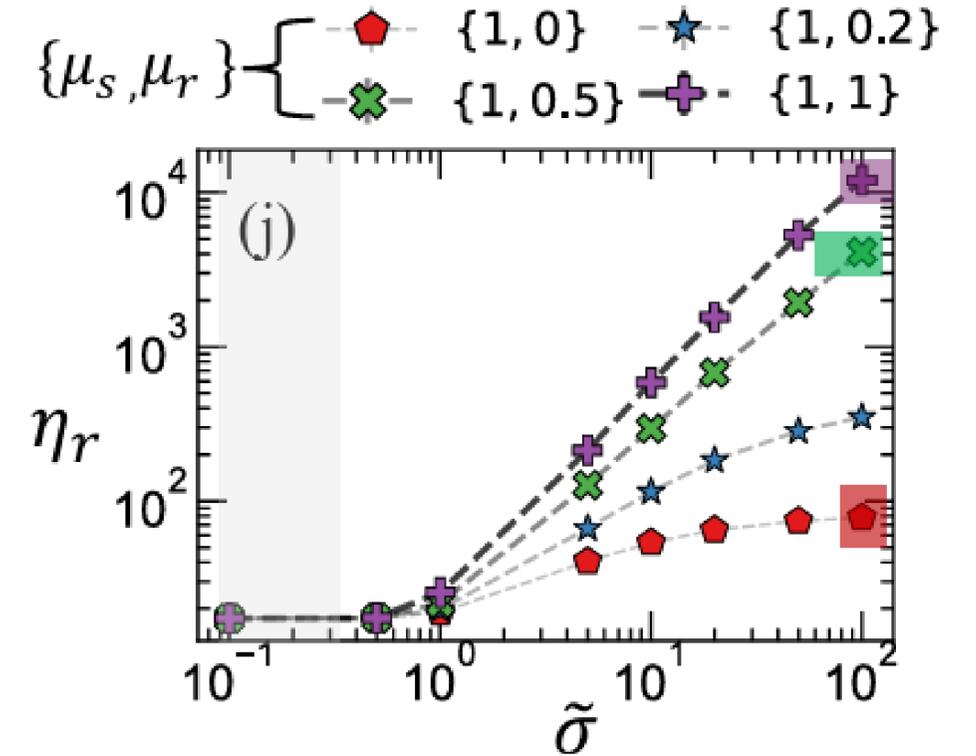
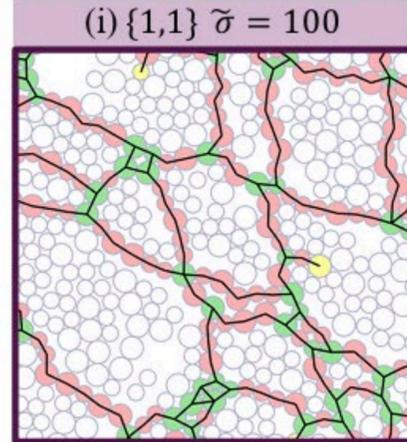
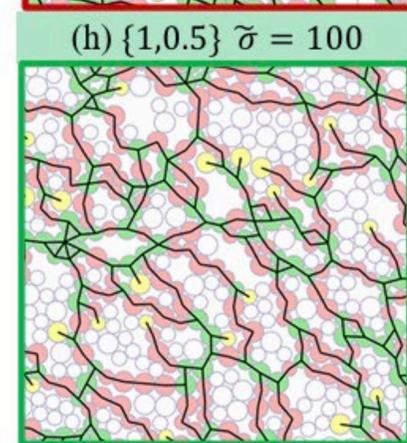
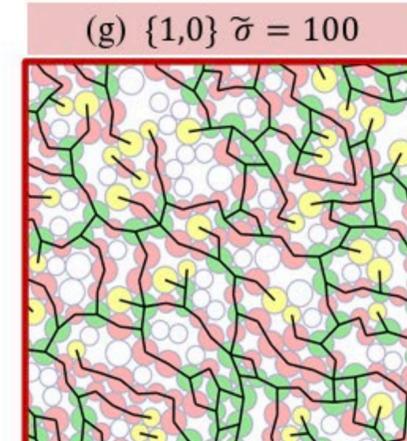
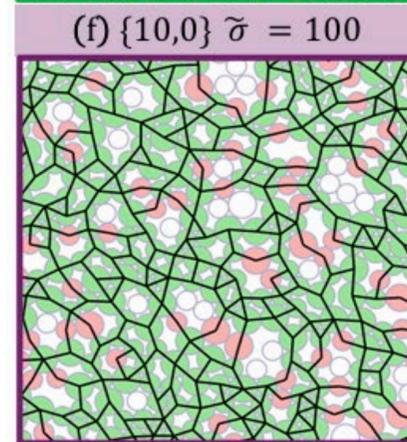
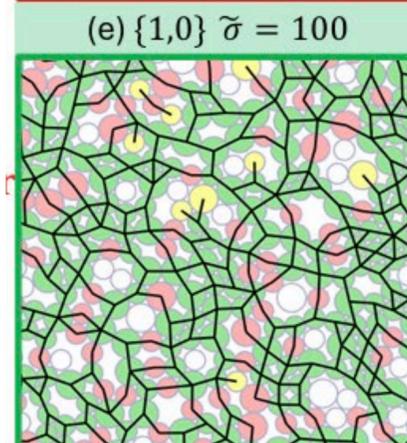
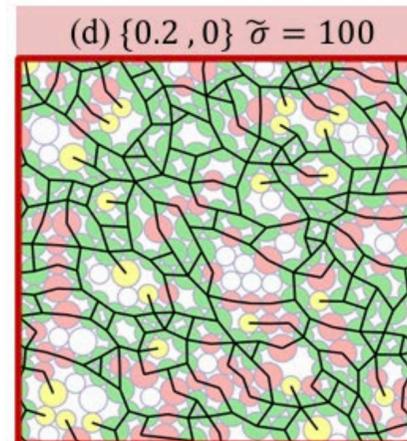
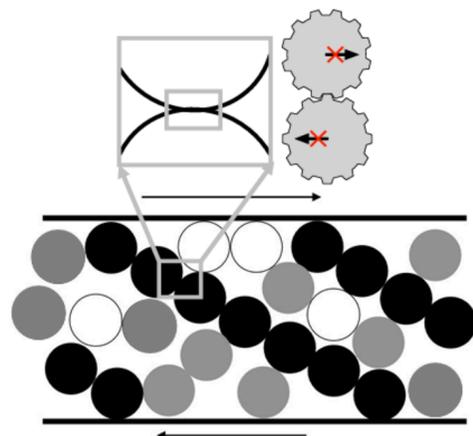
Sliding constraint only

Sliding and Rolling constraint

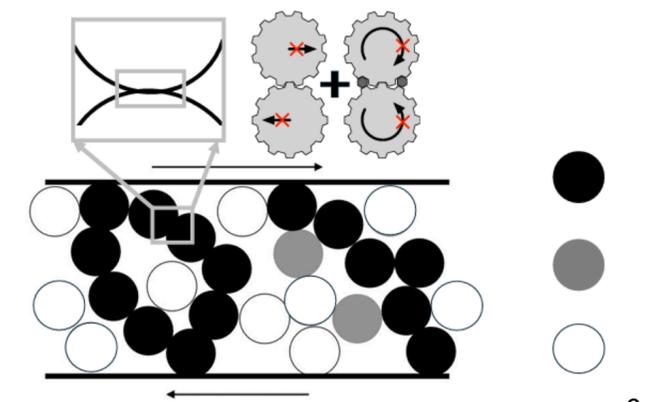
z_{μ}^{local} 0 1 2 ≥ 3



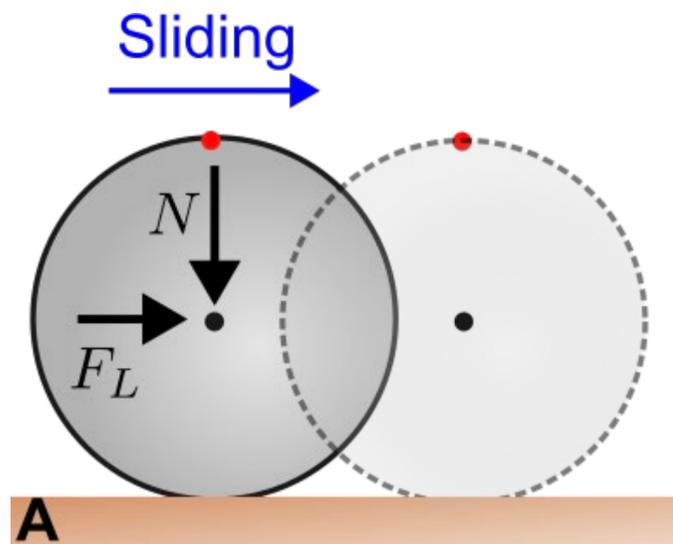
(a) Sliding constraint only



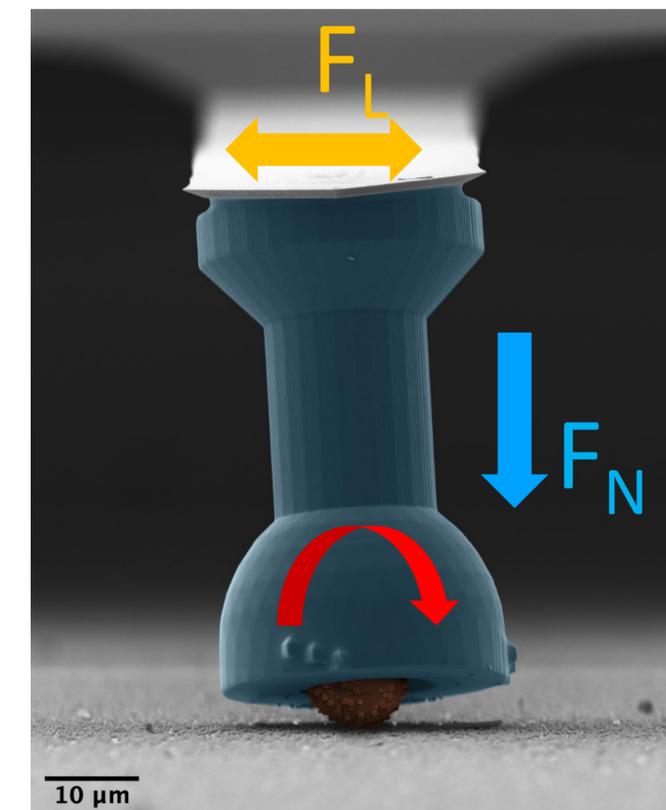
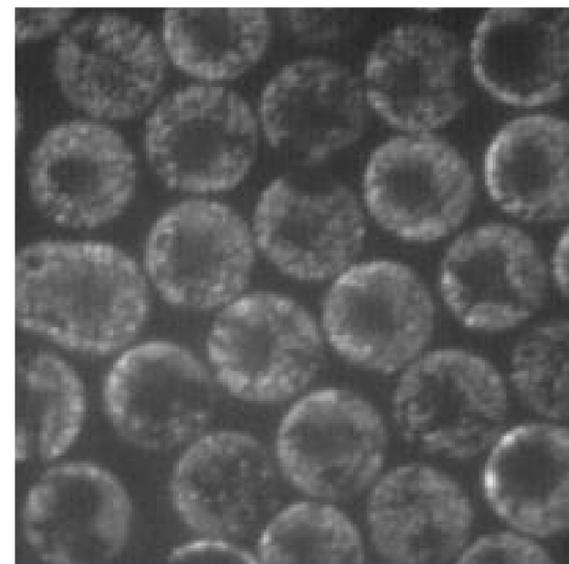
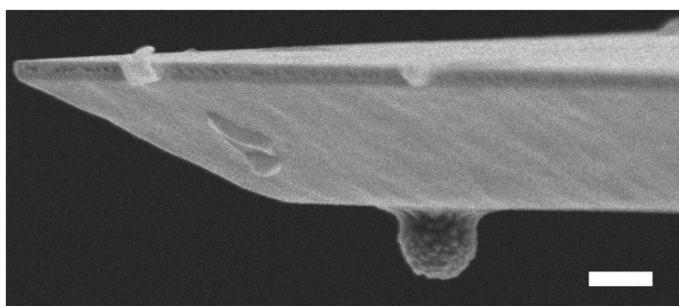
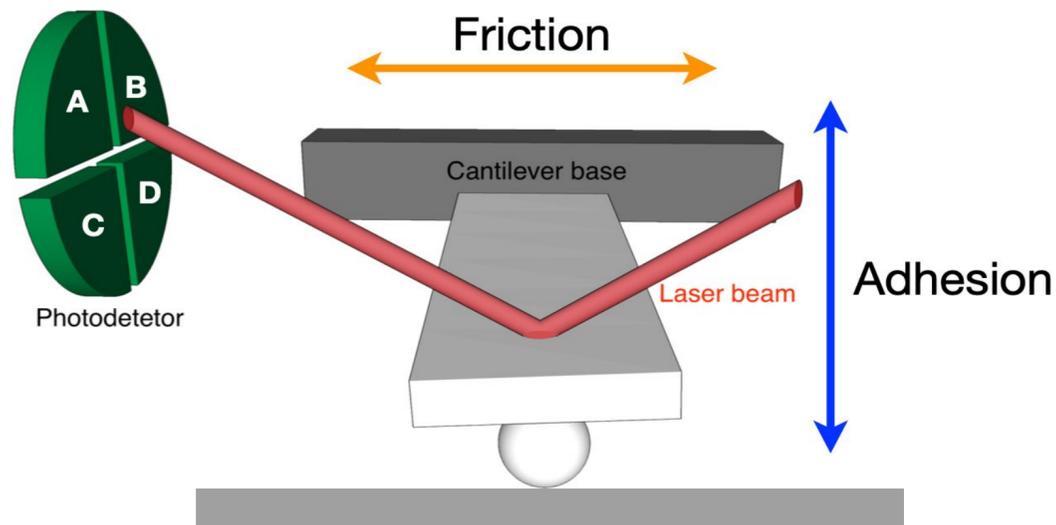
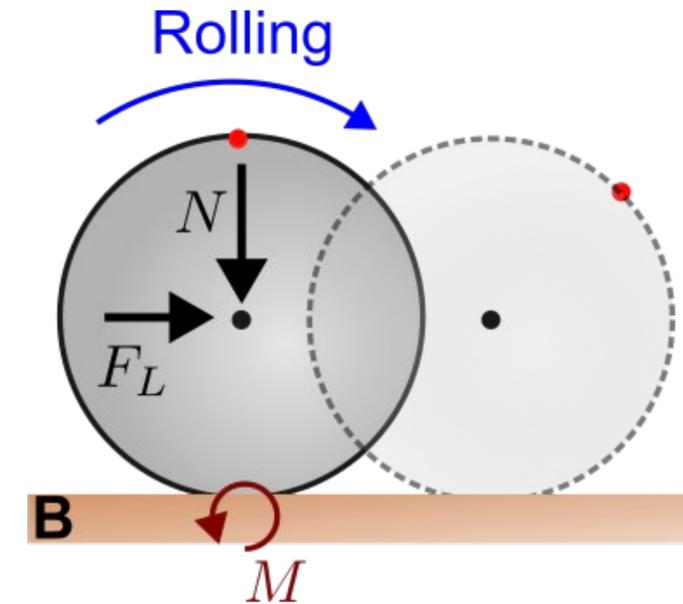
(b) Sliding and Rolling constraint



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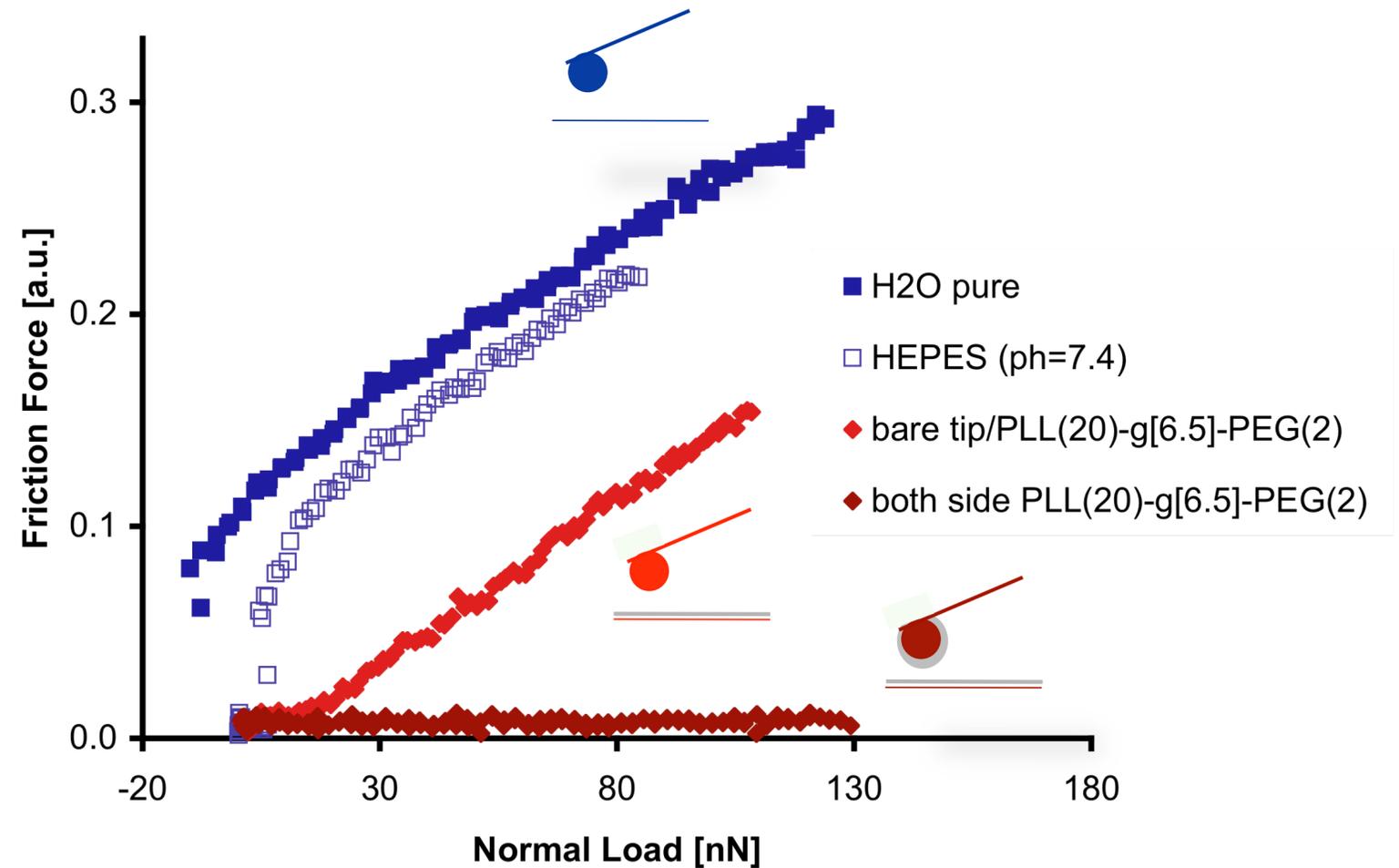
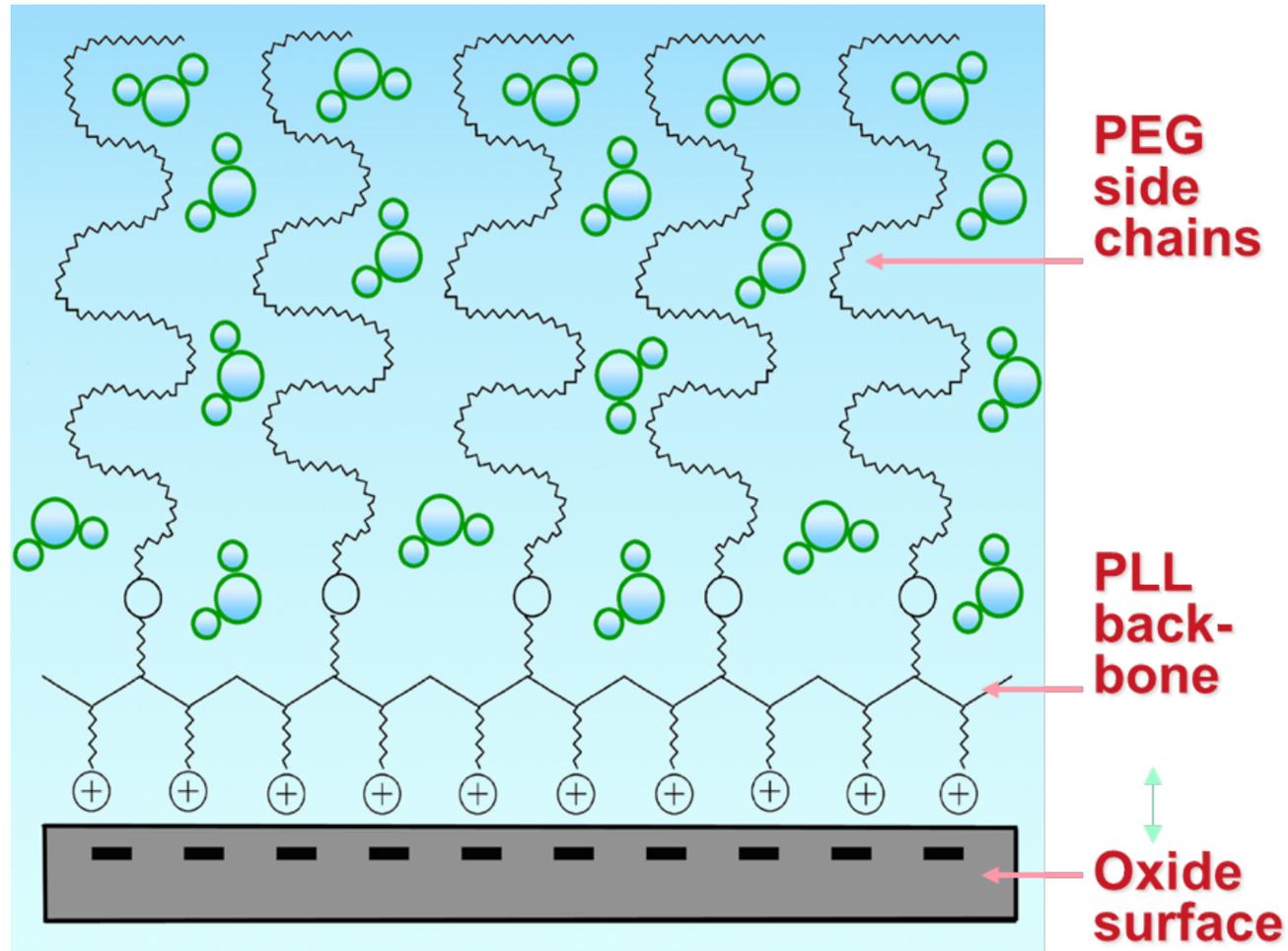


- Simultaneous detection of normal and lateral forces
- Detection of the kinematics of the contact (sliding, rolling or mixed)



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Coating surfaces with polymer brushes

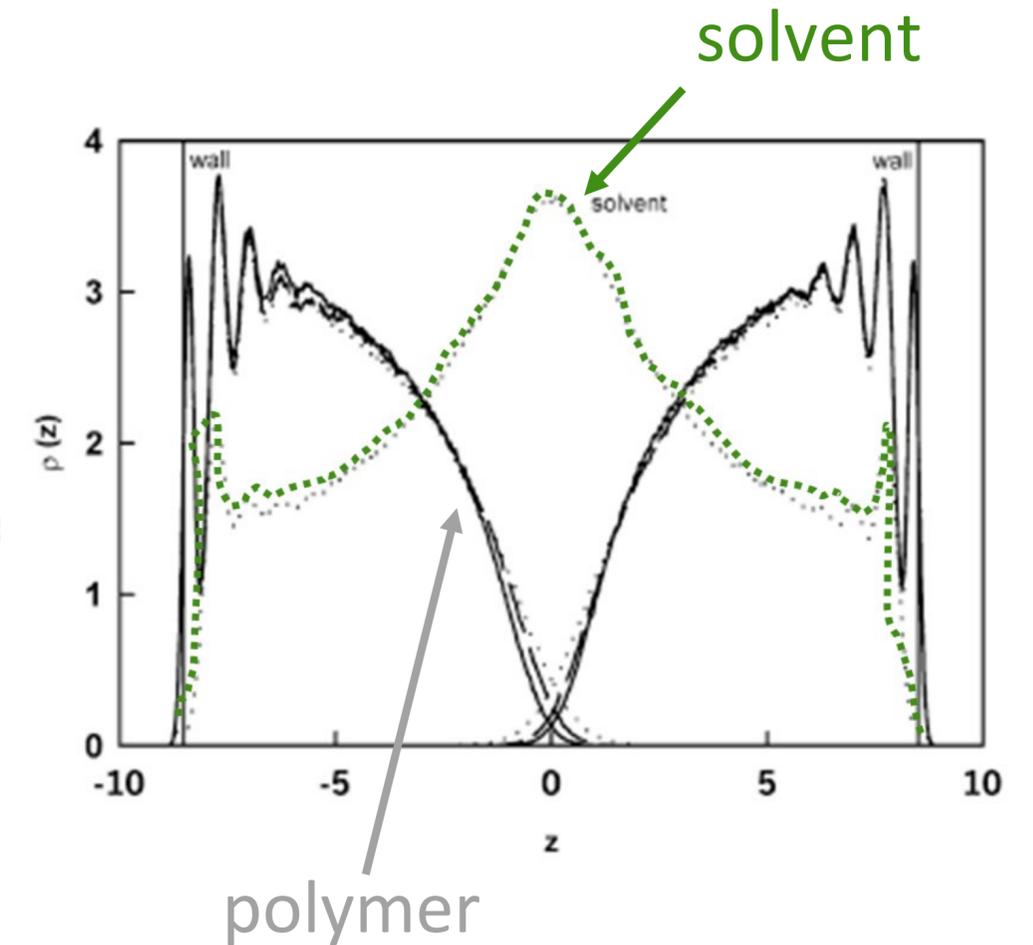
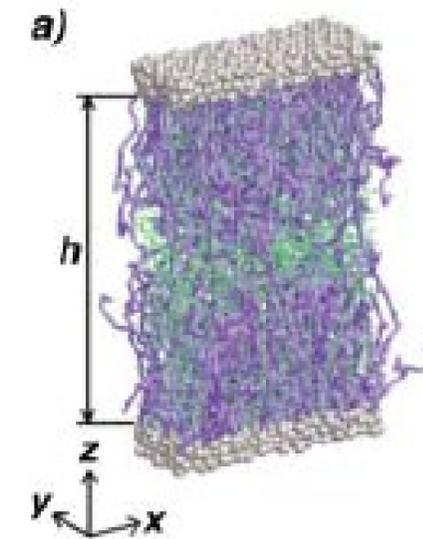
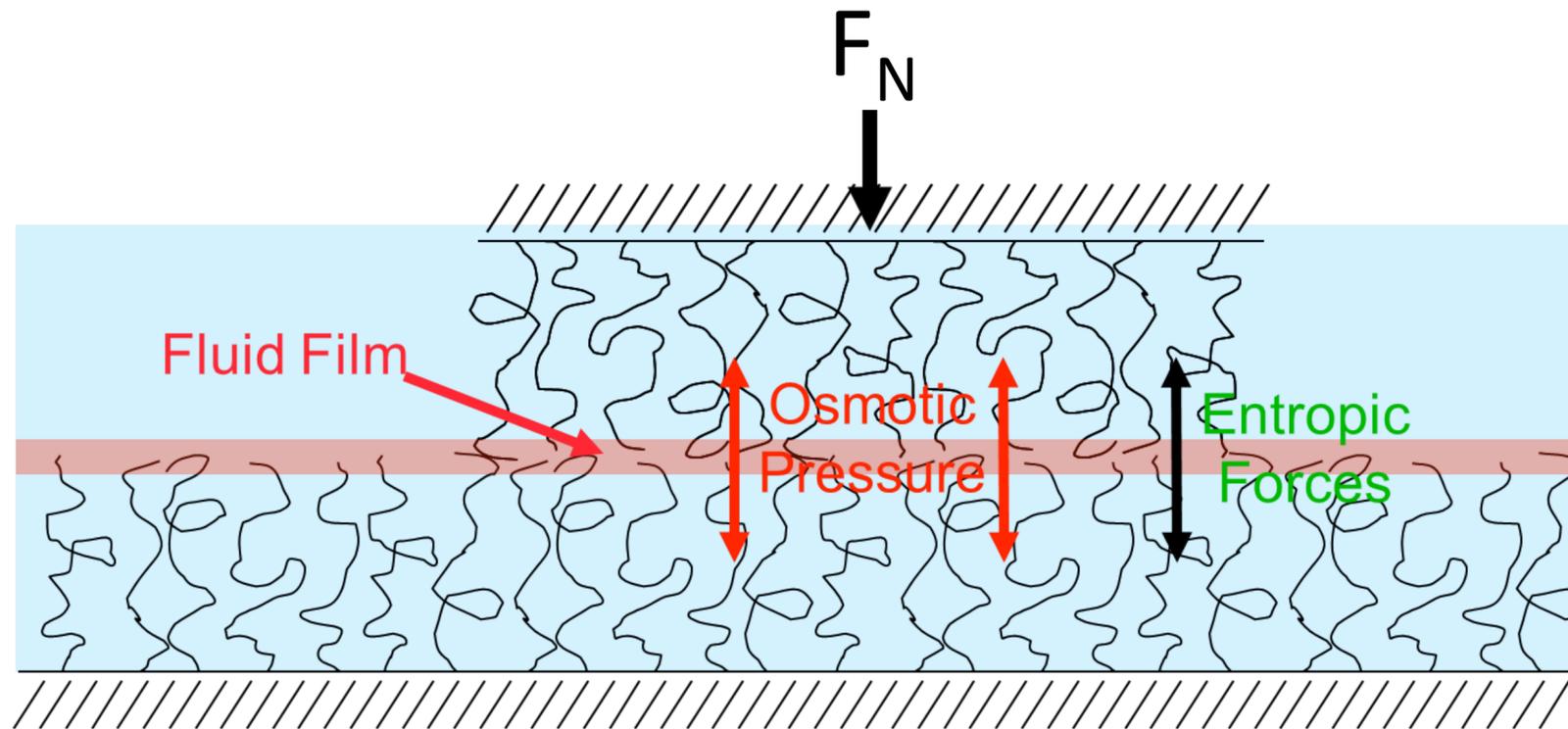


X. Yan et al. *Langmuir* 2004, 20, 423-428

Massive reduction of μ_s

Poly-l-lysine (PLL)-g-polyethylene glycol (PEG)

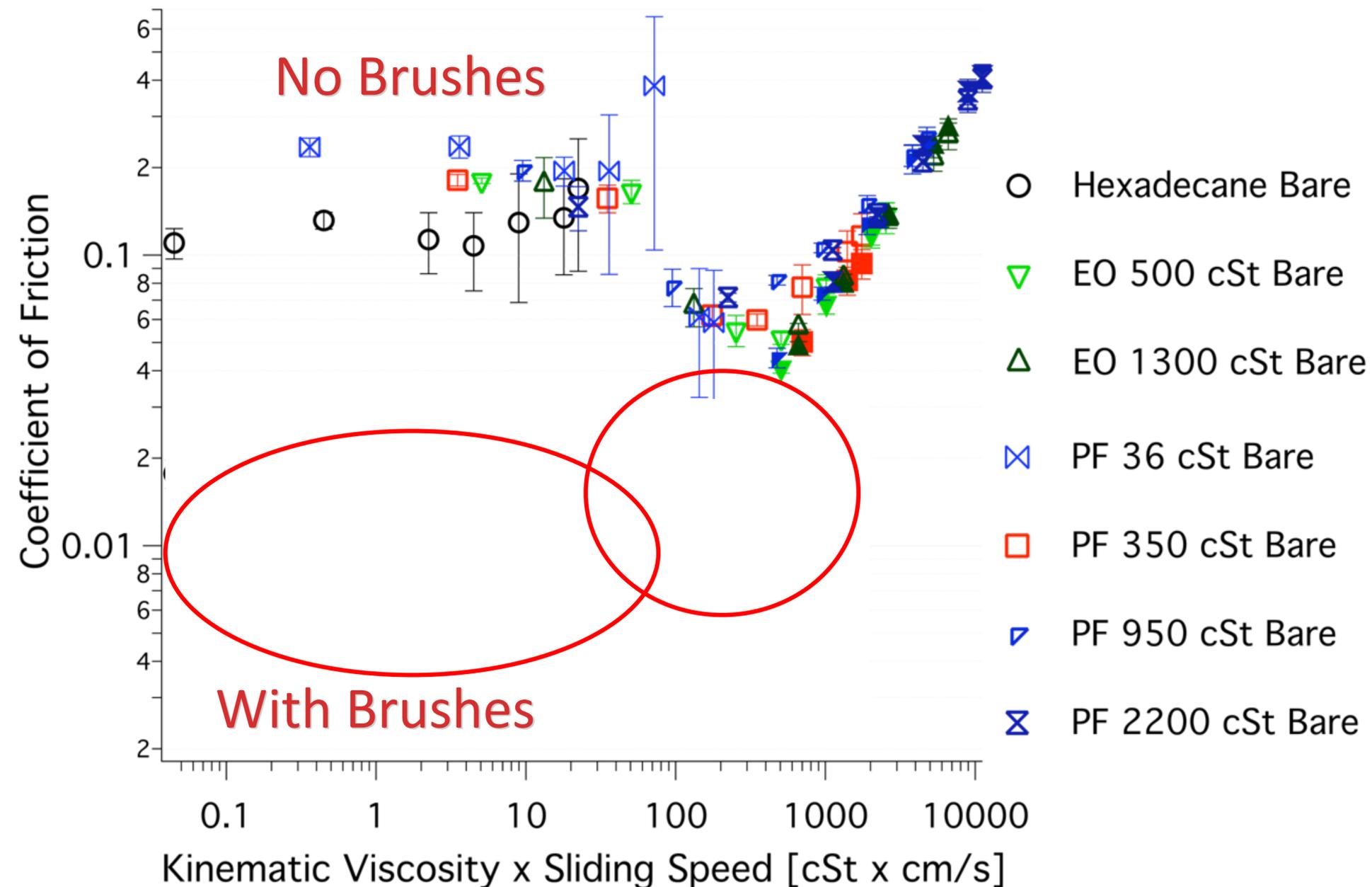
“Enforced” Fluid-Film Lubrication by Polymer Brushes



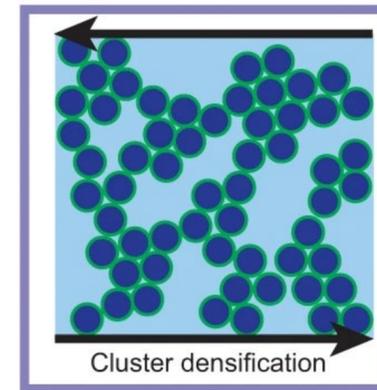
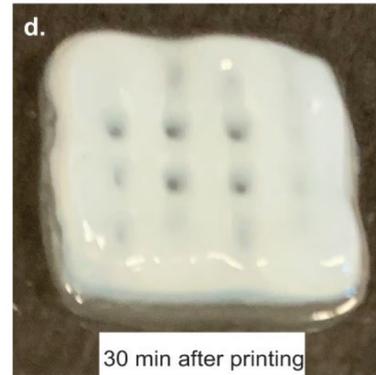
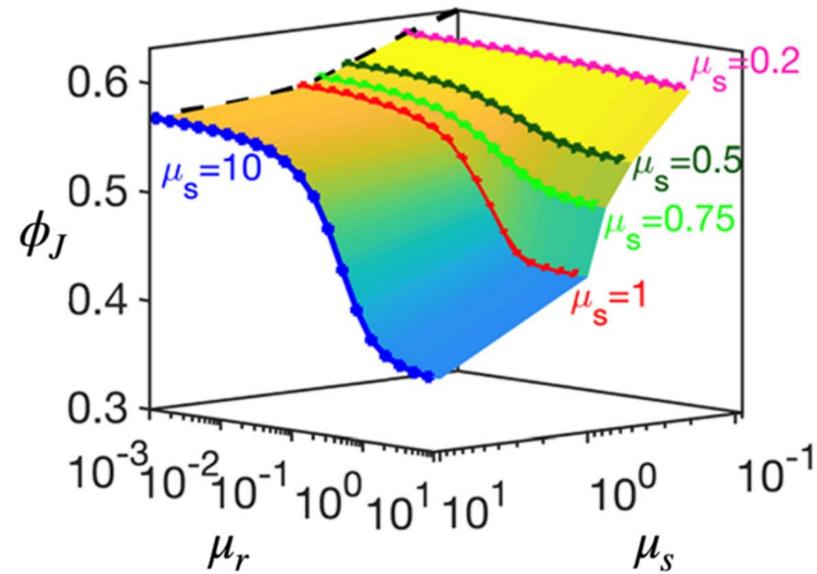
By retaining liquid within the brush and keeping the surface apart, polymer brushes reduce boundary lubrication coefficients μ_s

D. Irfachsyad et al. Phys. Chem. Chem. Phys., 2002,4, 3008-3015

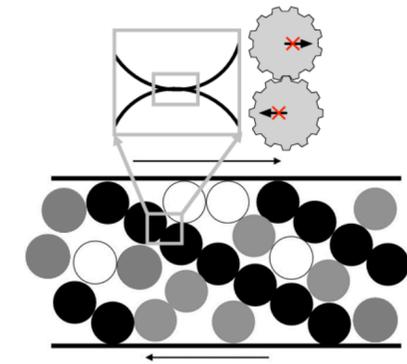
Stribeck Curve in Microtribometer: 7 Oils, Bare Borosilicate Against Brush or Si Wafer
 250nm (dry) Poly(dodecyl methacrylate), 20 mN, rotating, reciprocating, 20 cycles per point



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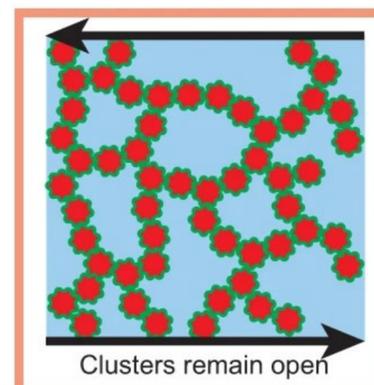
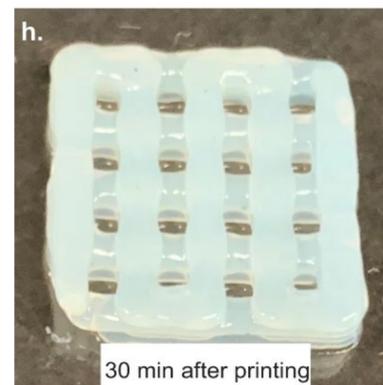
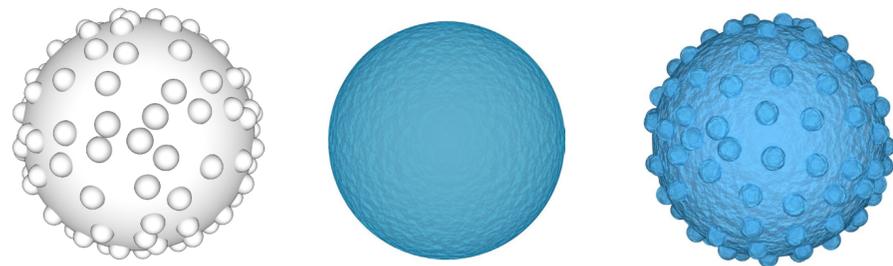
(a) Sliding constraint only



How do I engineer μ_s and μ_R during particle synthesis/fabrication to control ϕ_m ?

What is the role of adhesion and static friction in addition to μ_s and μ_R in materials such as gels?

Are there other rheological signatures of interest beyond steady shear viscosity in and how do we measure them?



(b) Sliding and Rolling constraint

